

# Local chromatic correction Arc & Final Focus

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- LCCO rationale
- Ring and Final Focus layout
- Hardware requirements
- Performances
- Conclusions

# Local Chromatic Correction Optic

LCCO based on the development of optics solutions that allow/rely on chromatic and harmonic corrections as local as possible. This has led to the development of:

## HFD ARC lattice.

The lattice has been optimized by introducing a “beta&phase-modulation” and relies on 4 sextupole families that results in a second-order achromat and nearly anharmonic lattice. The lattice is periodic over 5 Hybrid-FODO cells.

The optimized phase advance for ttbar operations is about  $100/74$ .

A weaker lattice that utilizes all the ttbar magnets that has a phase advance of about  $51/44$  is achromatic and anharmonic as well. It is considered to be used for Z operations and all modes that require a large momentum compaction.

Both lattices have a MA in excess of  $\pm 3\%$ ,

## Long Straight Section matching

The insertion of the straight sections is performed by requiring the “Transparency Conditions”.

This allows the virtually transparent insertion of any SS in a Ring, without any significant degradation of its characteristics (DA/MA, detuning etc), neither requiring the introduction of sextupole families.

The TCs can be applied for any given SS, provided that 4 quadrupoles/side are available to match the conditions.

## Final Focus.

LCCO requirements are fulfilled by correcting the low-beta IP chromaticity in the FF in both planes and nearly entirely.

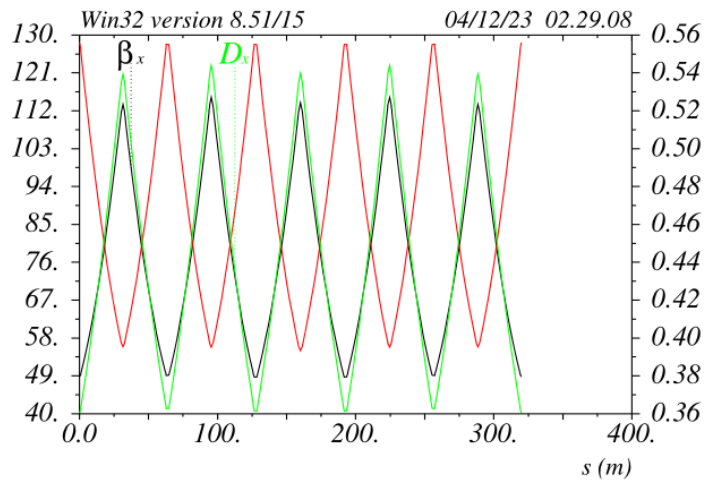
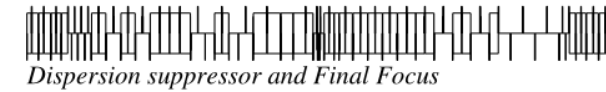
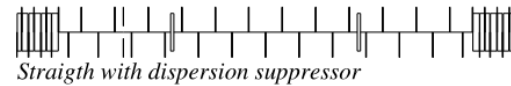
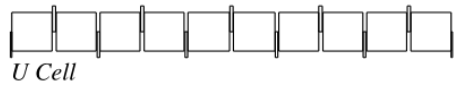
LCCO also results in the need of placing the Crab sextupoles in a nearly “chromatic-free” region: the FF outer ends.

This solution has been developed for the SuperB and has been adopted by CEPC as well.

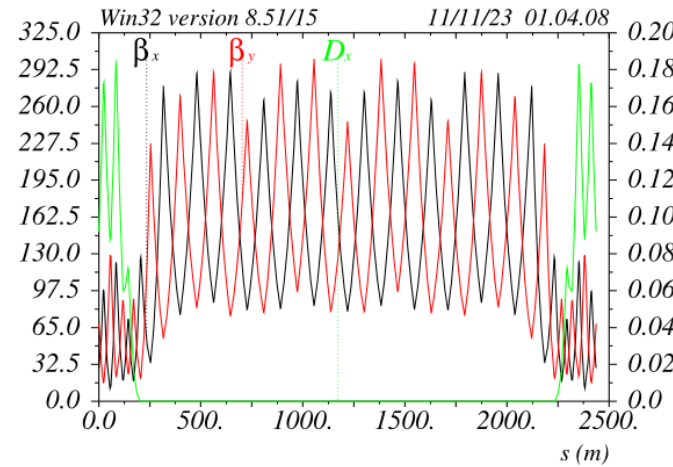
V\_74 optic matches the baseline layout:

- LSS 2032m long as baseline
- ARCs bending radius as baseline
- FF section length set to match overall ring circumference: 90658.609m (tunnel length 90657.609)

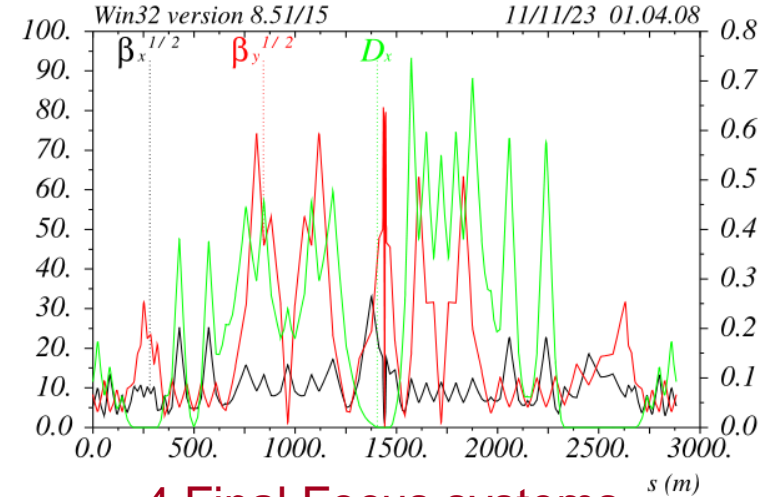
Specialized LSS optics (injection, collimation, RF) presently not included.



30 cells/octant



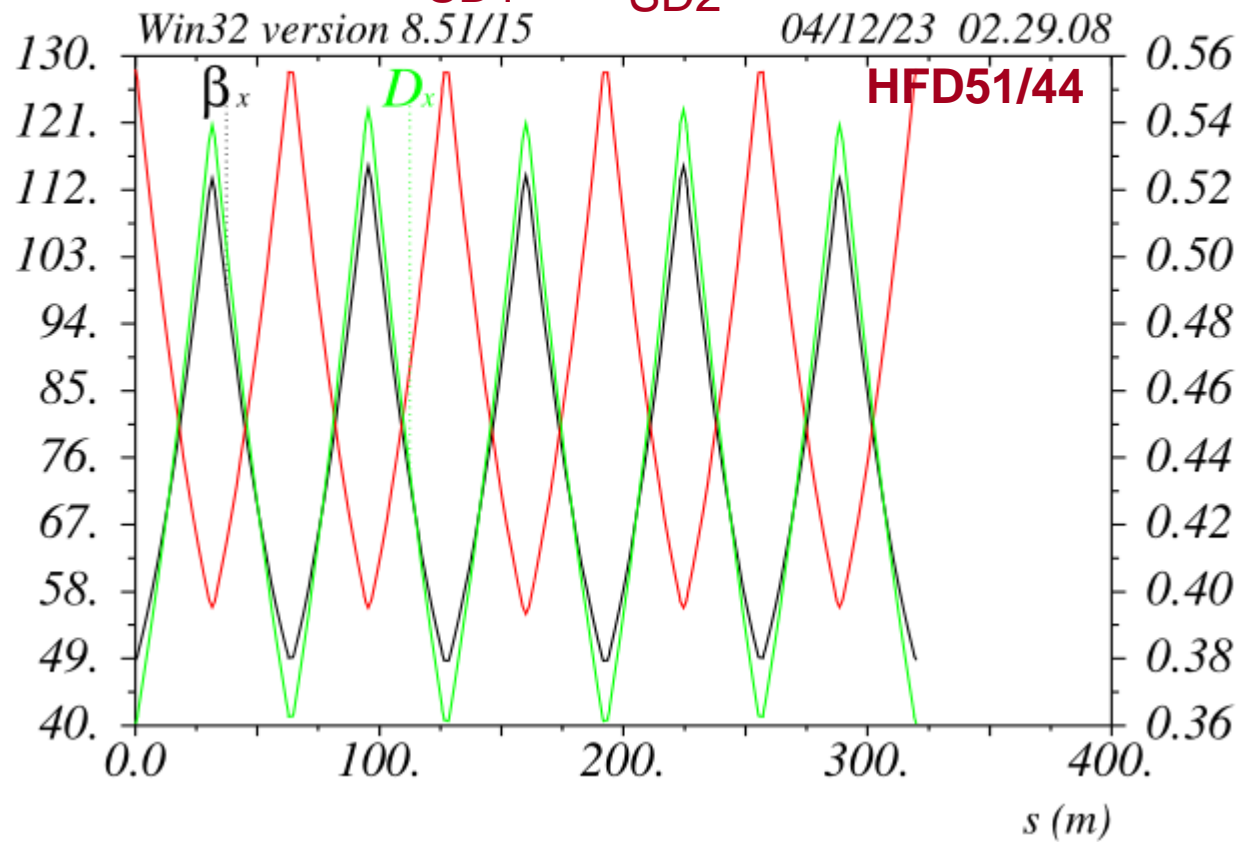
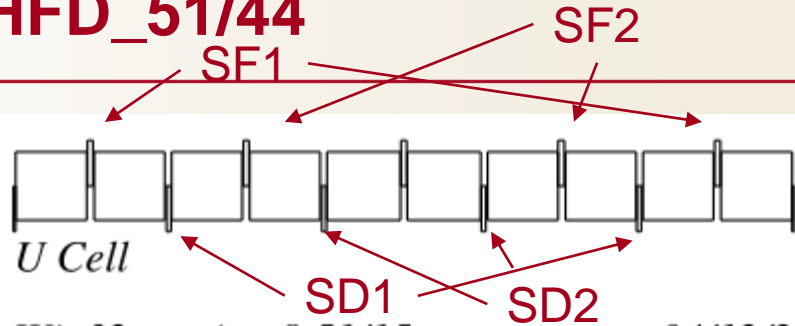
4 Long Straight Sections



4 Final Focus systems

# HFD\_51/44

# Z mode



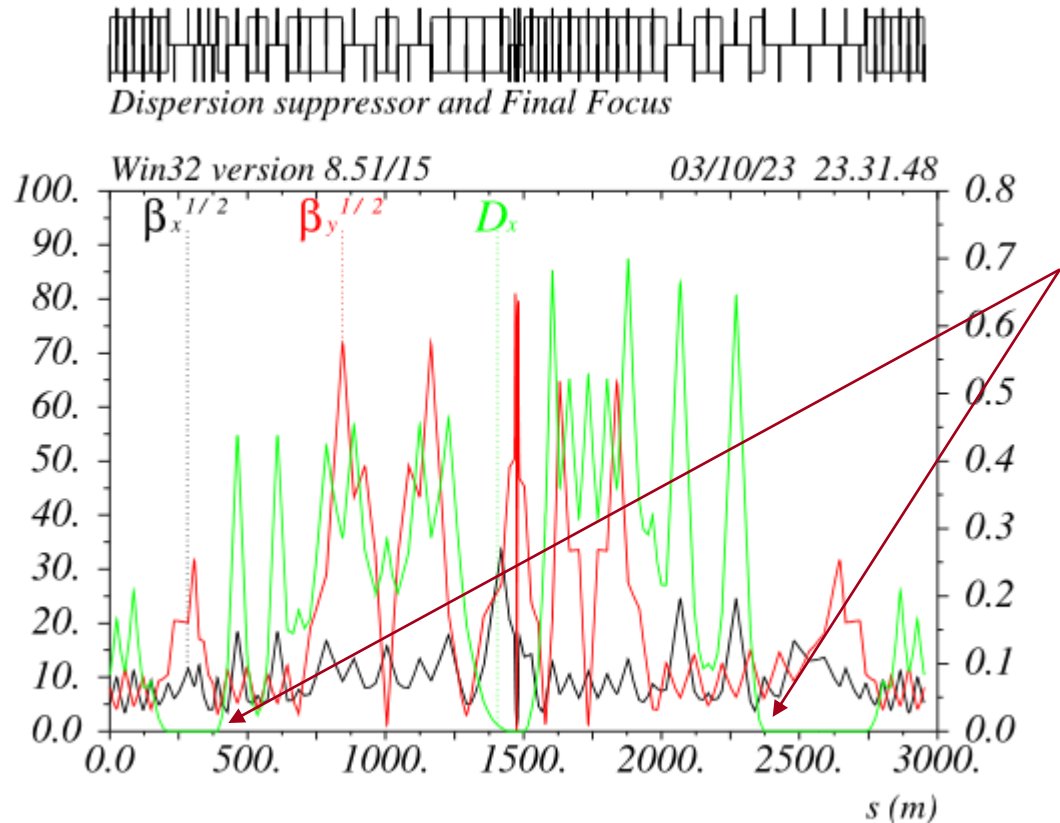
Given the additional degree of freedom from the 4 sexts families, good tunes working points do exist almost continuously.

HFD\_51/44 delivers:

$E_x = 0.70\text{nm}$      $\text{Alphac} = 3.30\text{e-}5$   
( $E_x = 0.69\text{nm}$      $\text{Alphac} = 2.94\text{e-}5$  for full ring)

Muy has been chosen as best compromise between chromaticities, detunings and sensitivity to collective effects.

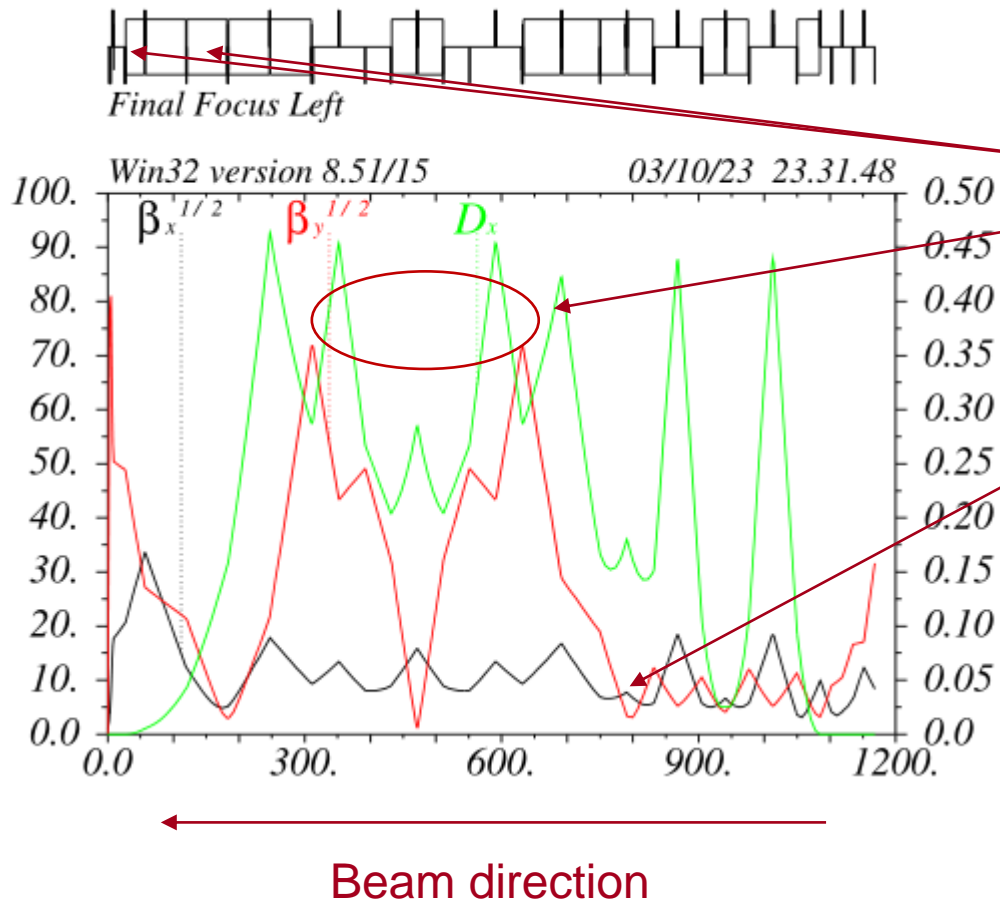
Peak betas are very similar to the HFD100/74 (Long9090 FODO has twice larger betas wrt Short9090)



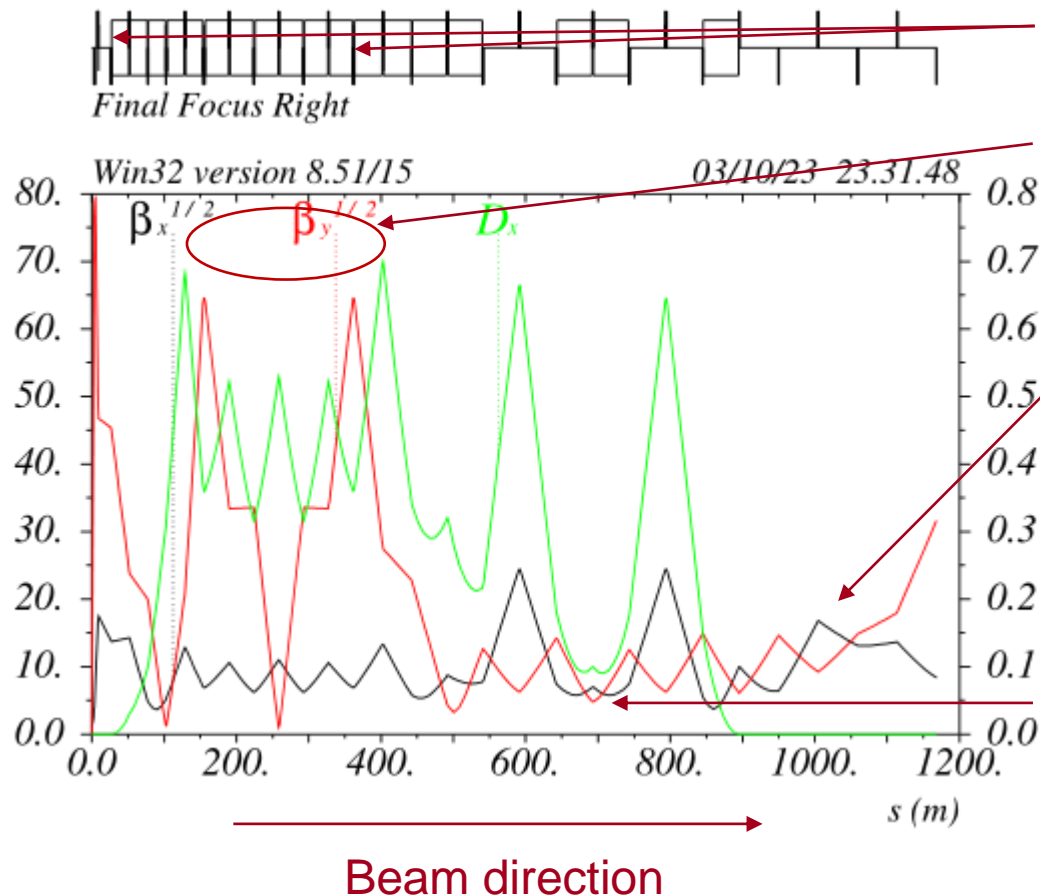
The FF geometry is adjusted in order to recover entirely the beams separation. Dipoles ARCs modification is not necessary.

Beams start to split @300m and are back @2300m  
(Present separation in the ARCs is set to 40cm)  
CCsX\_Left section is short and has “strong bends”  
CCsY\_Left section is long and has “weak bend”  
CCsY\_Right section is short and has “strong bends”  
CCsX\_Right section is long and has “weak bend”

Details in next slides

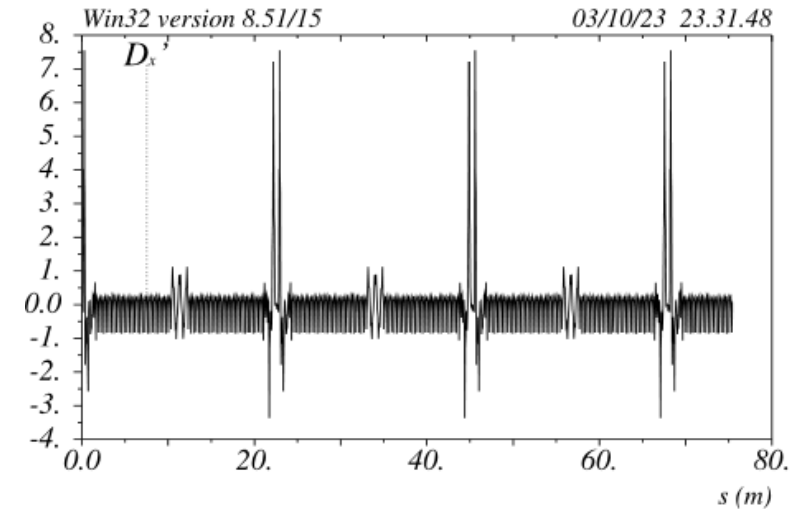
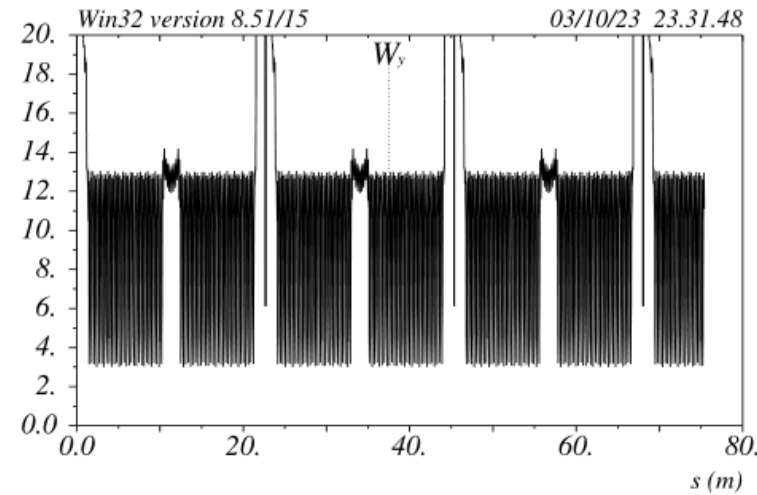
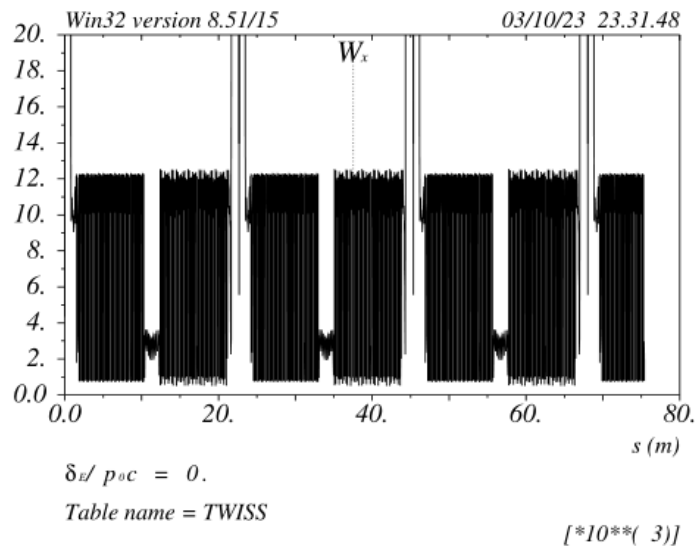


- Last 3 dipoles EC~130KeV
- CCSy optic has the largest dispersion (so far) for a given bend angle in the  $-I$ , presently  $D_x=0.303m@SDs$
- “Standard” non-linear optimization is performed as usual
- Betas&Alfas at IP-phase sextupoles are optimized to reduce the DA reduction from Crab sextupoles
- CCSy/x\_L/R lengths and ratio between their total bend angles are optimized to have maximum dispersion on CCSy\_Left and minimum overall emittance growth and radiation
- CCSy sextupoles (0.6m long) are very weak  $Ks\_madx \sim 0.7$  @ttbar,  $Ks \sim 0.9$  @Z. In fact ARCs sextupoles can be used in the FF as well



- All dipoles in the CCSy have same field, best configuration to recover the beams separation
- CCSy optic has the largest dispersion (so far) given the above requirement in the  $-I$ , presently  $D_x=0.370m@SDs$
- “Standard” non-linear optimization is performed as usual
- CCsX has been shortened and pushed back, helping to recover the geometry. Incidentally this has originated a very long dispersion free straight section,  $\sim 400m$  when included the ARC DS part
- Two drift sections about 100m long are also present in the CCsX “-I”
- Alfay in the CCSx\_LR is not zero to symmetrize the F\_LR non linear optic





Chromaticity in the ARCs is periodic and about 12 in both planes

This is extremely beneficial to reach and maintain top performances in a very short time

No sextupole families are needed

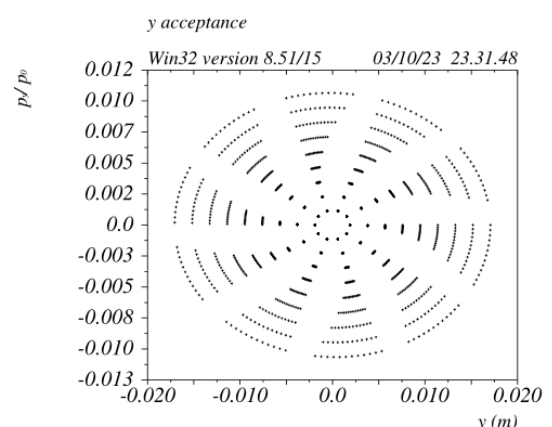
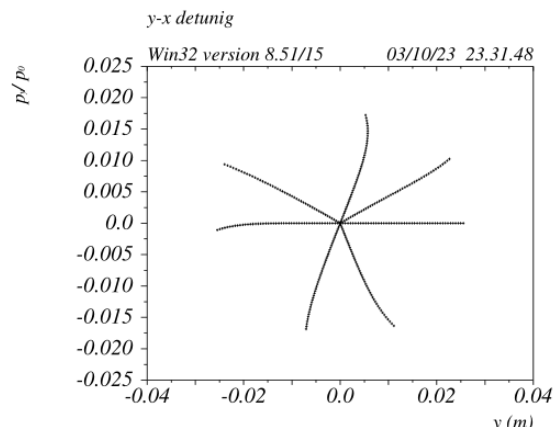
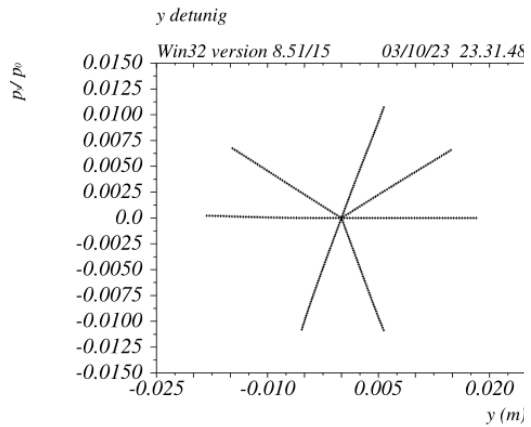
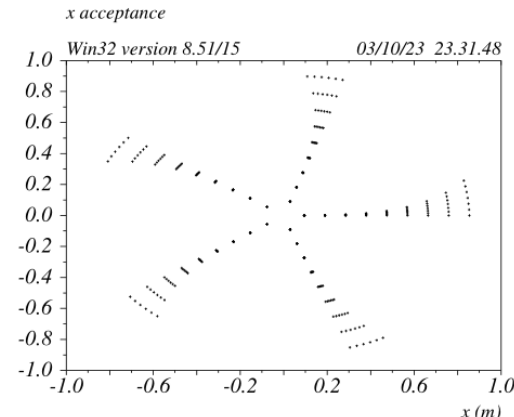
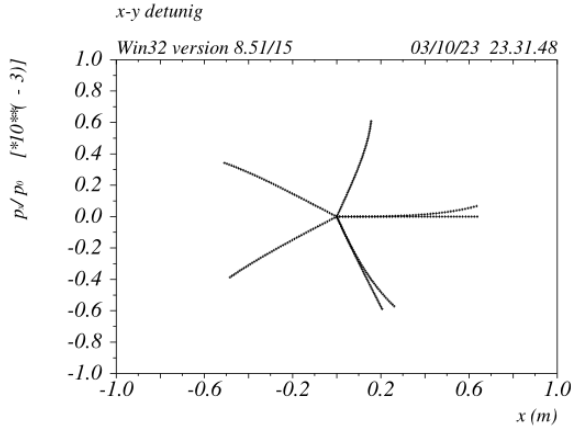
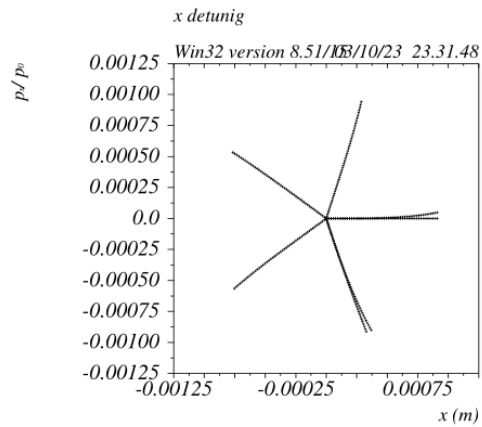
Because the “Full Achromat” FF property, there is no need to change the ARCs&FF

sextupoles (and CS) setting when the beta-squeeze is done with the beta-matching quads

This is extremely beneficial to reach top performances, it will be extremely useful to level the luminosity on the 4 IPs as well.

# Full ring transverse DA

v\_67 ttbar optic



On energy dynamic is linear.  
“Resonances” are virtually not existing.  
Extremely favourable dynamics to minimize BeamBeam degradation (DS)

The quest/dream for a “quasi” time-independent trajectory is at reach!

# Cancelation of the Energy dependent Y & XY detuning with decapoles: restoring the CCs sexts “-I” condition for off energy particles

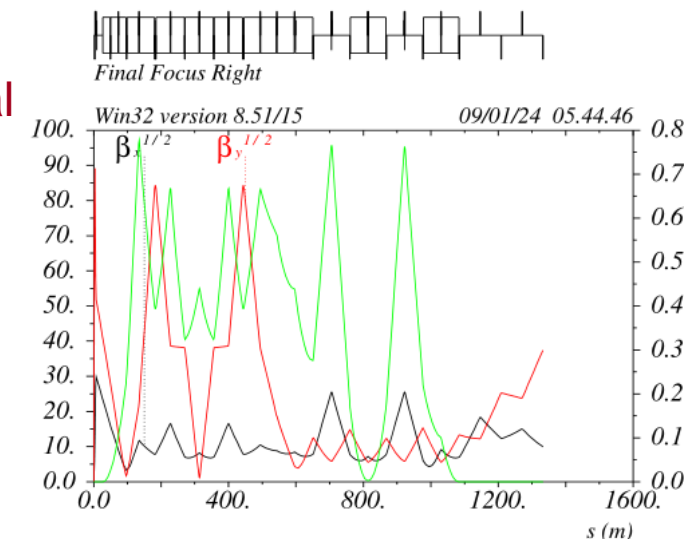
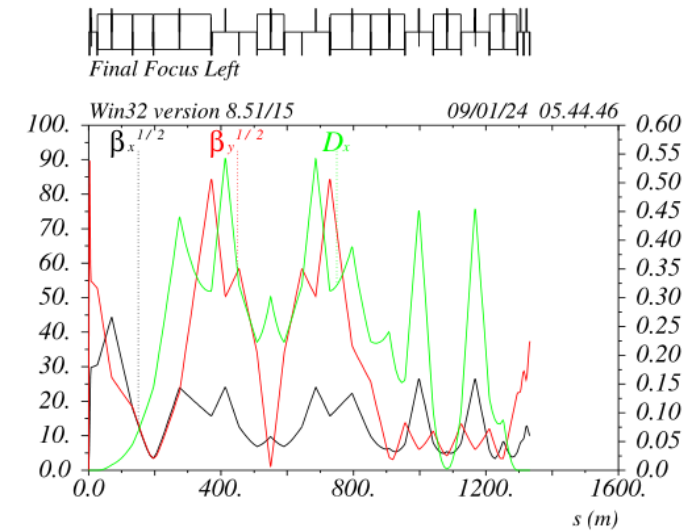
The trick adopted is to use the Left and Right decapoles pairs to cancel “globally” the detuning:  
FFL&R instead of FFL and FFR individually.

- 1) CCSy\_Left decapoles are negative and cancel de\_xy\_detuning
  - 2) CCSy\_Right decapoles are positive and cancel de\_y\_detuning
  - 3) CCSx\_L&R decapoles are positive and cancel de\_x\_detuning
- Betax/y@CCSyL/R are set to maximize the decapole effectiveness:

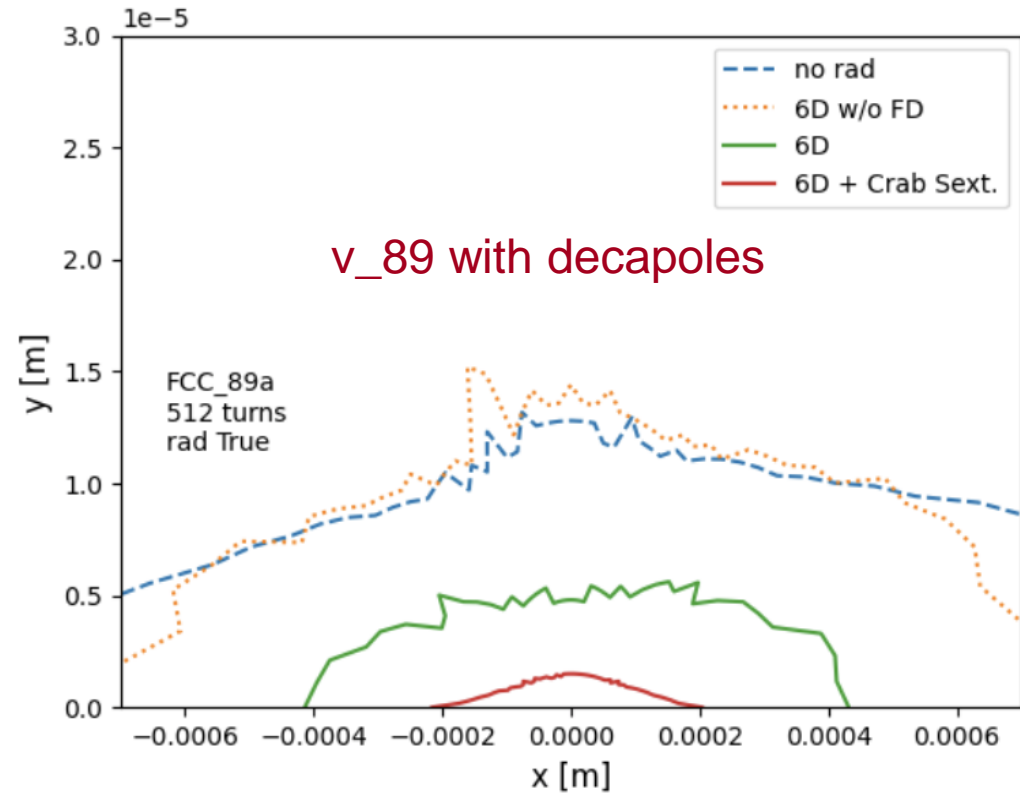
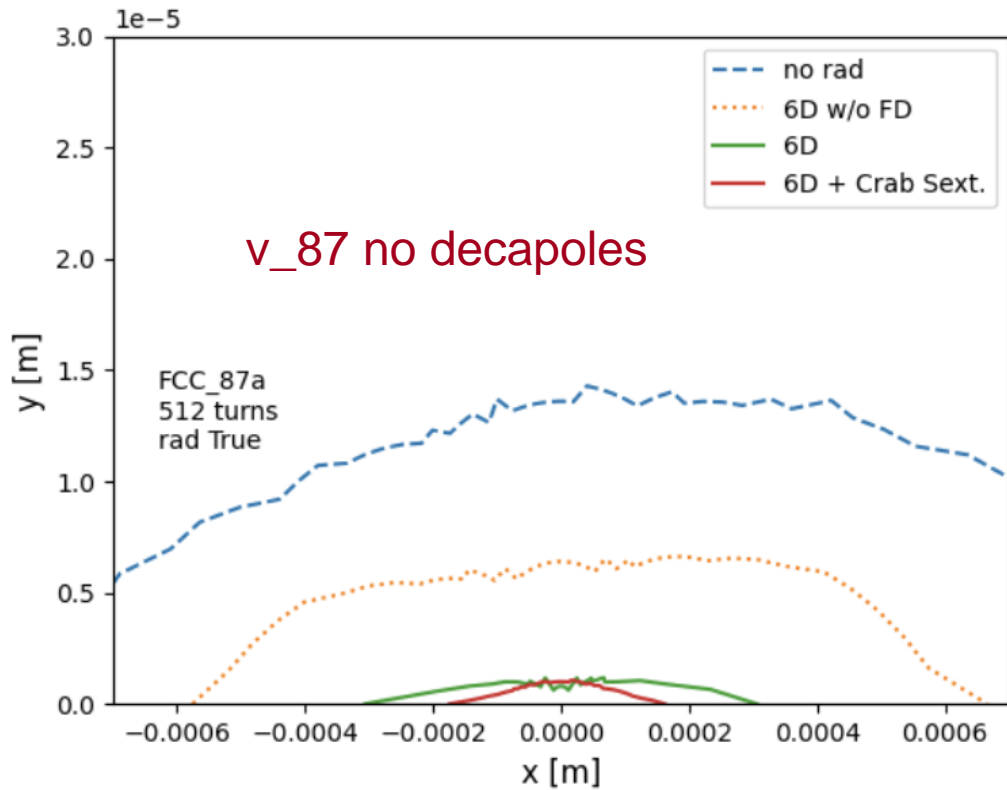
|                                 |          |                    |
|---------------------------------|----------|--------------------|
| CCSy_L: betay=7100m, betax=250m | dx=0.30m | K4L_DECDDL ~ -2200 |
| CCSy_R: betay=7100m, betax=65m  | dx=0.40m | K4L_DECDDR ~ +3000 |
| CCSx_L&R betay~30, betax~650    | dx~0.60m | K4L_DECFL&R ~ +500 |

Given the very high order of the aberration the decapoles pairs are very orthogonal

The transverse (mainly vertical) residual nonlinearities of the CCSy decapoles are canceled altogether because the opposite sign of the Left/Right ones.  
There are no side effects on the DA and on on\_energy detunings  
The third order chromaticity is weakly affected, this results in a small change in the IP\_phase sextupoles settings. Makes the x-IP\_phase\_sextupoles 10% weaker



# Dynamic aperture without and with Synchrotron Radiation

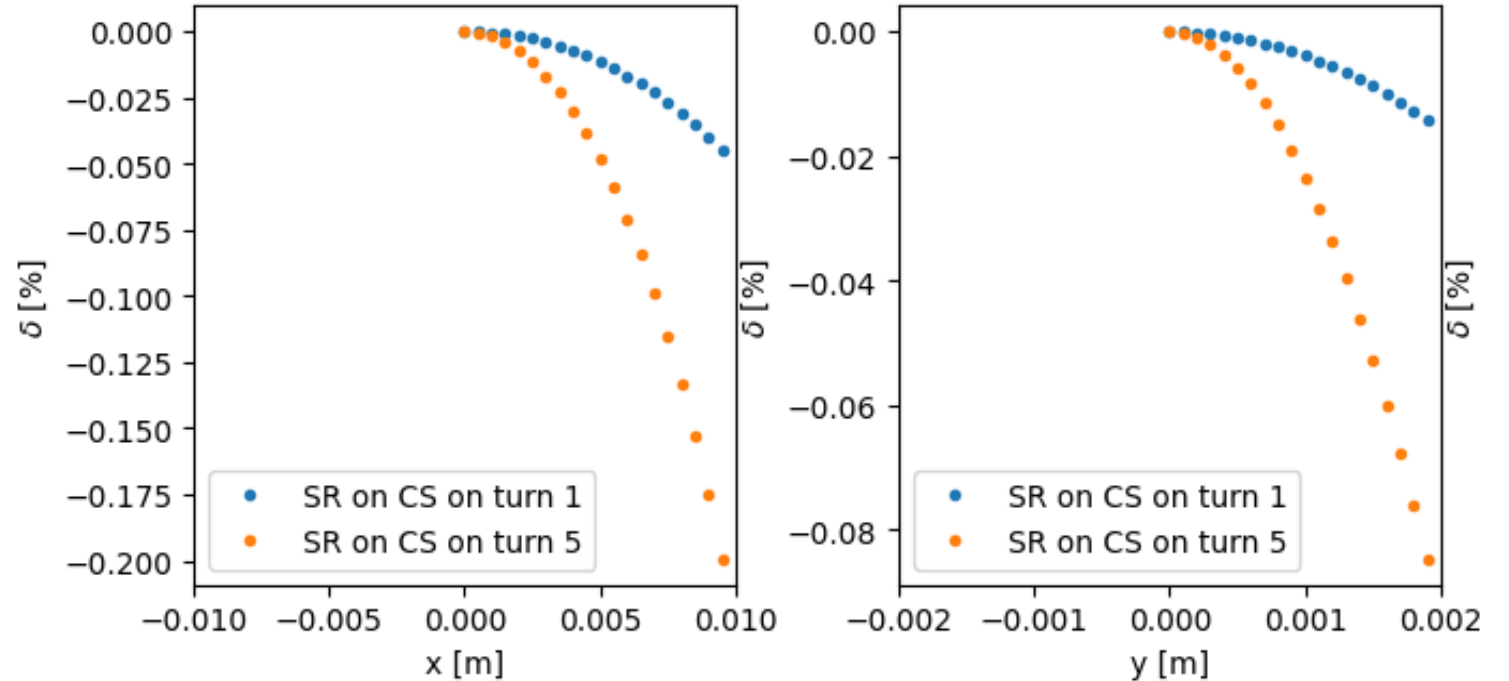


The effectiveness of the decapoles is evident  
This is probably the first time that the degradation due to the quadrupoles-SR and FD-SR in particular is very effectively addressed

# Energy loss due to Final doublet radiation

Energy loss induced by final doublet SR only.

Similar for the two lattices.  
After 160 turns the beam loses 2% and is lost out of MA.  
The RF helps to recover the energy loss and the DA might improve by optimizing the RF voltage

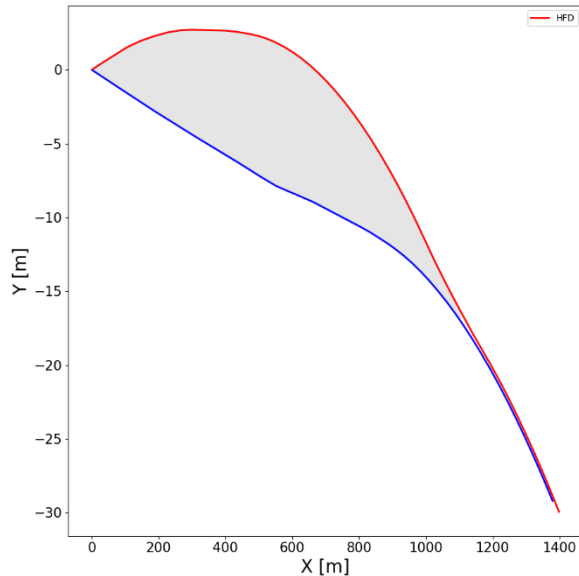


# FF layout

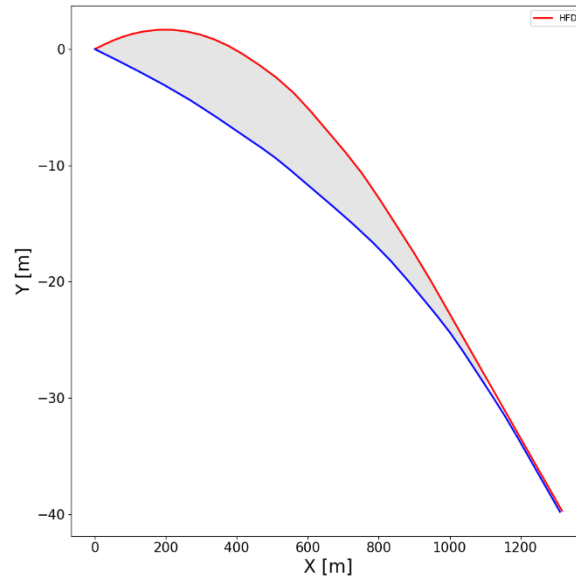
v\_89



IP offset wrt to baseline is around 11m



Baseline: area 6640m<sup>2</sup>  
Max separation 9.6m



LCCO: area 4960m<sup>2</sup>  
Max separation 7m

There are no reverse bends thus simplifying the SR radiation handling for the distributed absorbers

The stronger dipoles are in the CCSy\_R just downstream the IP, they are anyway about 10% weaker wrt the ARCs ones.

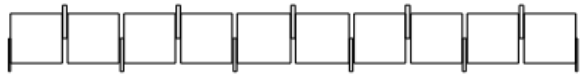
The “Soft bend” upstream the IP is about 230m long and has an  $E_c \sim 130\text{KeV}$  @ttbar

Overall the ratio  $\text{FF\_Eloss}/\text{FF\_bend\_angle}$  is very similar to the ARC one.

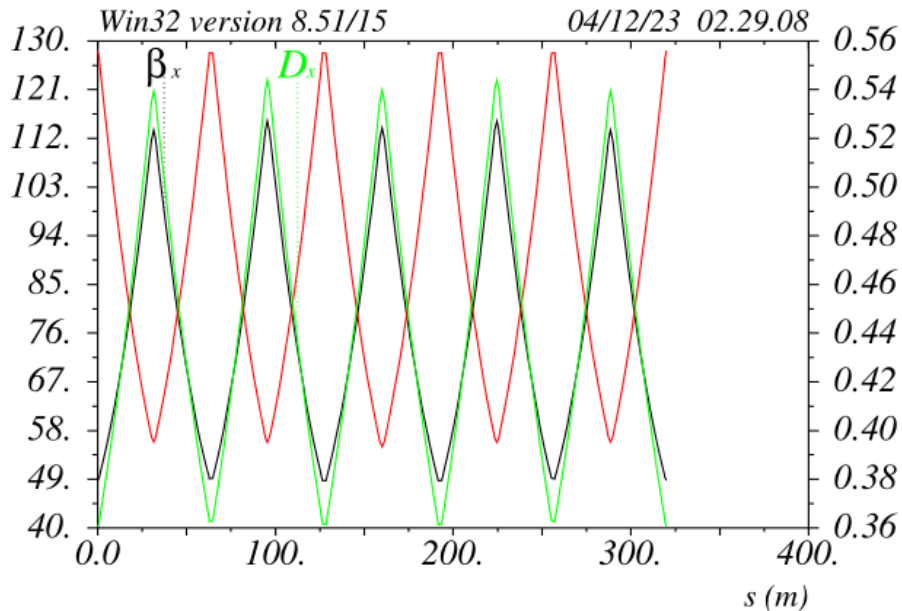
There are no superconducting magnets required except the FD ones (this might change if some zero-leakage quadrupoles are needed). FF sextupoles@ttbar have  $k$ \_values around 1 (1.5@Z) and are 60cm long. FF quads are shorter and weaker wrt ARC's

# ARC layout

# Z and ttbar mode



U Cell



- The arc is a standard FODO sequence with two missing sextupole for every 10 quads.
- BPMs are placed at each sextupole location (between sext and quad)
- The sextupoles are the ones presently designed and the foreseen trimming coils are all what is needed for orbit and optic correction.
- Sextupoles are 0.40/0.50m long, power consumption is < 5MW
- Quads are 2.4/1.8m long and should consume about 5Kw each, 2240 per ring are needed => 23MW@ttbar
- Dipoles are about 29.6m Long

In the case of HTS option the sextupoles are wrapped around the quadrupoles.

In principle by shifting the arc longitudinally by 30m, the QF will overlap with the QD.

In this case it could be possible to use a 1.8m twin quad as in the baseline + a 0.6m QF on one side only.

Pros and cons of this possibility should be carefully quantified.

# Beam parameters

|                     | units    | V22@Z 45.6 GeV       | LCCO-89@Z 45.6 GeV        |
|---------------------|----------|----------------------|---------------------------|
| circumference       | m        | 9.1174e+04           | 9.0659e+04                |
| momentum compaction |          | 2.8448e-05           | 2.8968e-05                |
| tunes               |          | 214.26 214.38        | 198.20 174.30             |
| chromaticity        |          | -0.0183, -0.0782     | -0.2942 1.0593            |
| damping time        | seconds  | 0.7102 0.7117 0.3549 | 0.8037 0.8037 0.4018      |
| energy spread       |          | 3.9182e-04           | <b>3.7148e-04</b>         |
| bunch length        | mm       | 3.2                  | <b>3.0</b>                |
| hor. nat. emittance | pm rad   | 706                  | <b>676</b>                |
| energy loss / turn  | MeV/turn | 39.0                 | <b>34.3</b> (lower power) |
| RF voltage          | MeV      | 200                  | 200                       |
| harmonic number     |          | 135000               | 135000                    |

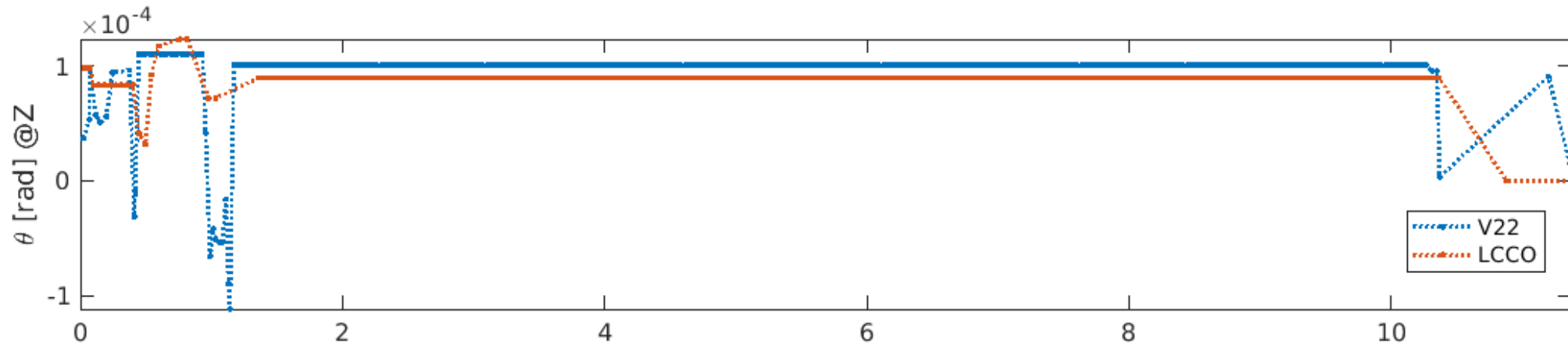
Python Accelerator Toolbox tracking: 6D = including synchrotron radiation and RF  
 Quantum diffusion is not included in the following studies (available).

<https://github.com/atcollab/at>  
 Fully benchmarked with MADX-PTC



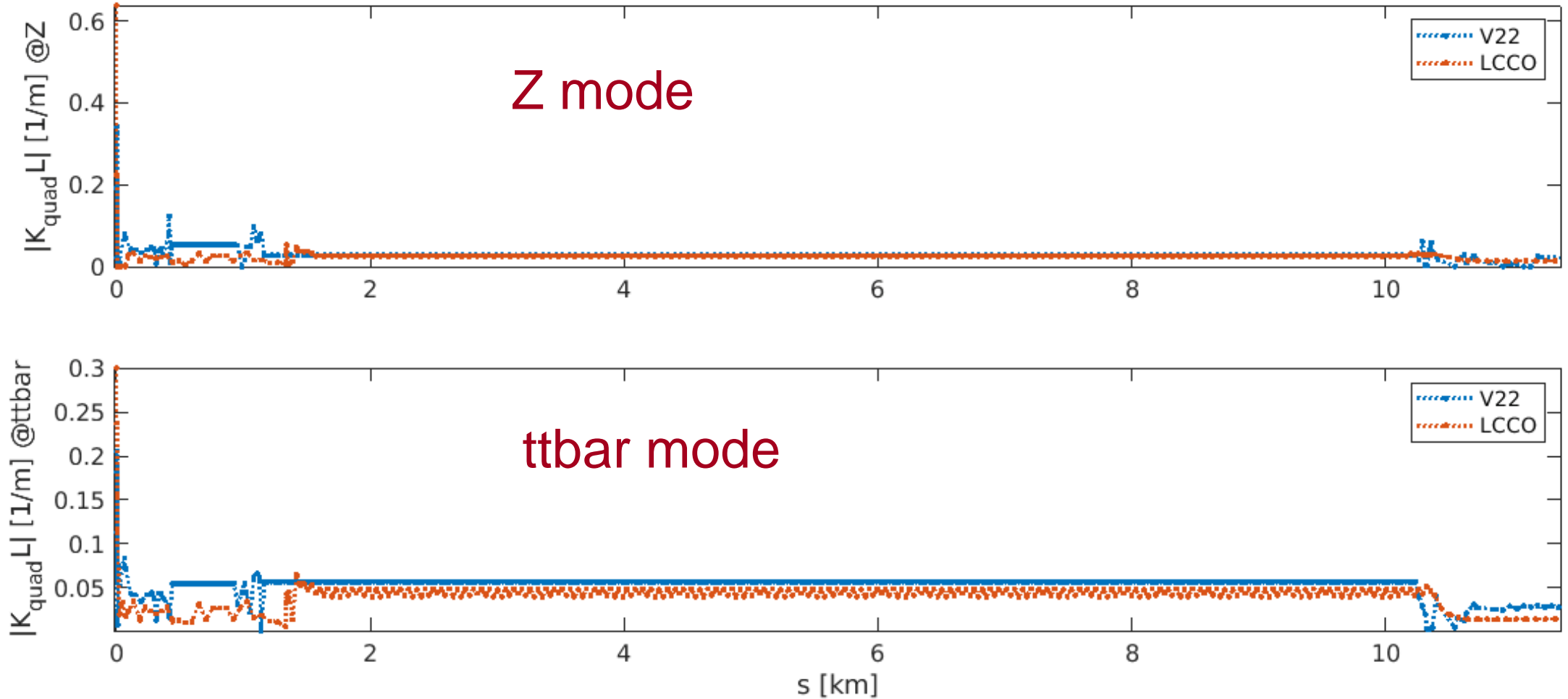
# DIPOLE FIELDS (1 octant)

Z&ttbar mode



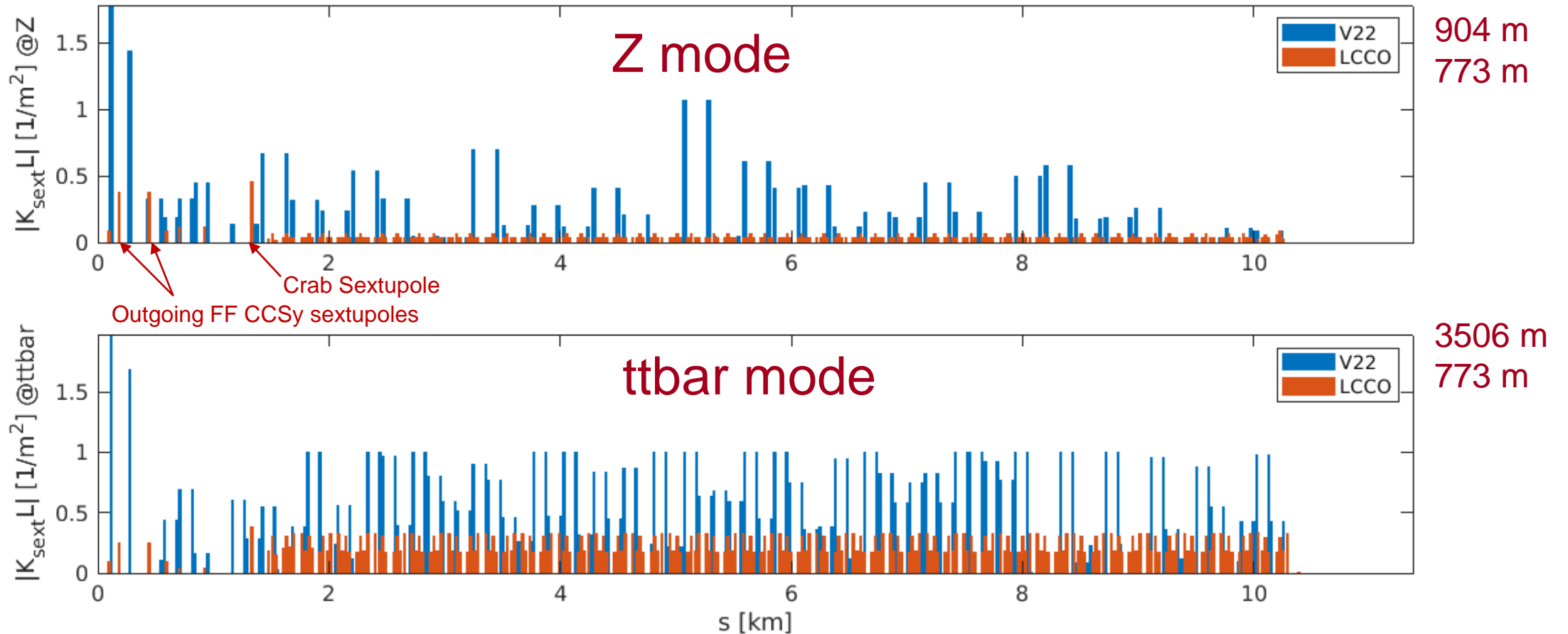
No negative angle bends for LCCO optics  $\rightarrow$  easier synchrotron radiation absorption scheme

# QUADRUPOLE GRADIENTS (1 octant)



Lower gradients for quadrupoles for LCCO optics (apart final doublet)

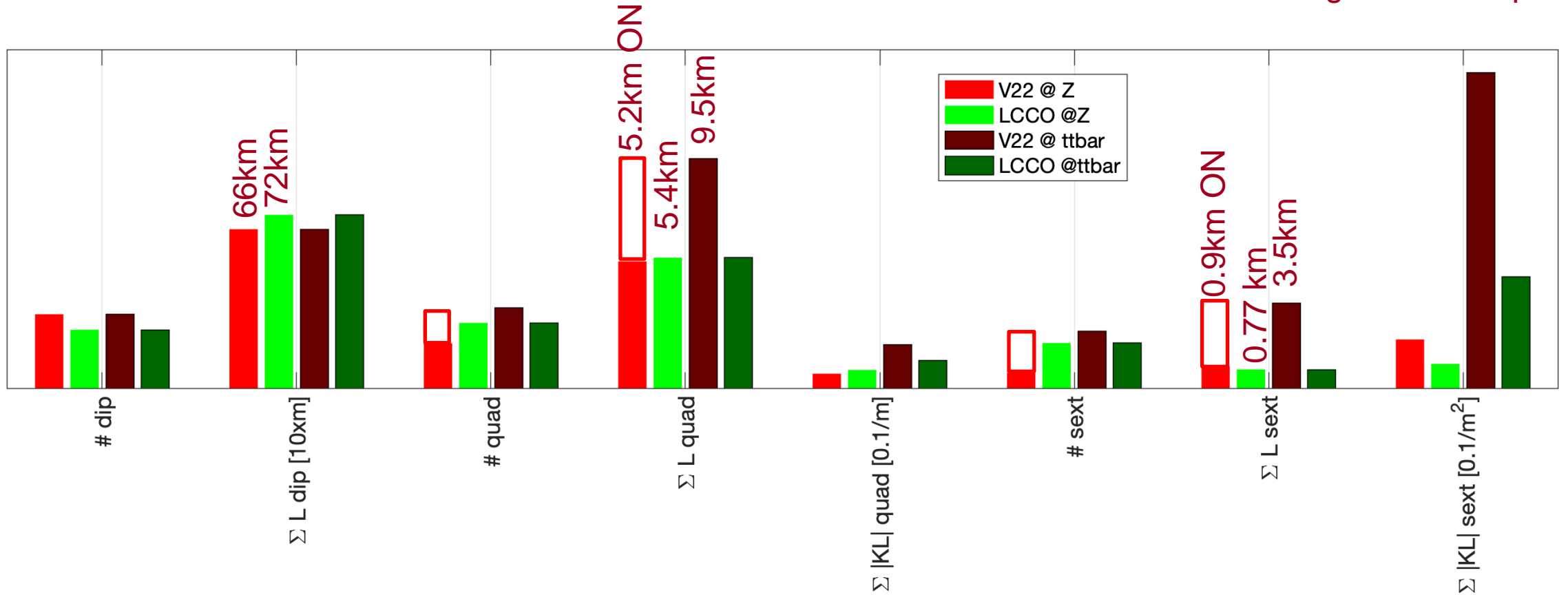
# Sextupoles gradients (1 octant)



Smaller sextupole gradients → Usually better performances.

# Number of magnetic elements and gradients

Including Crab sextupoles

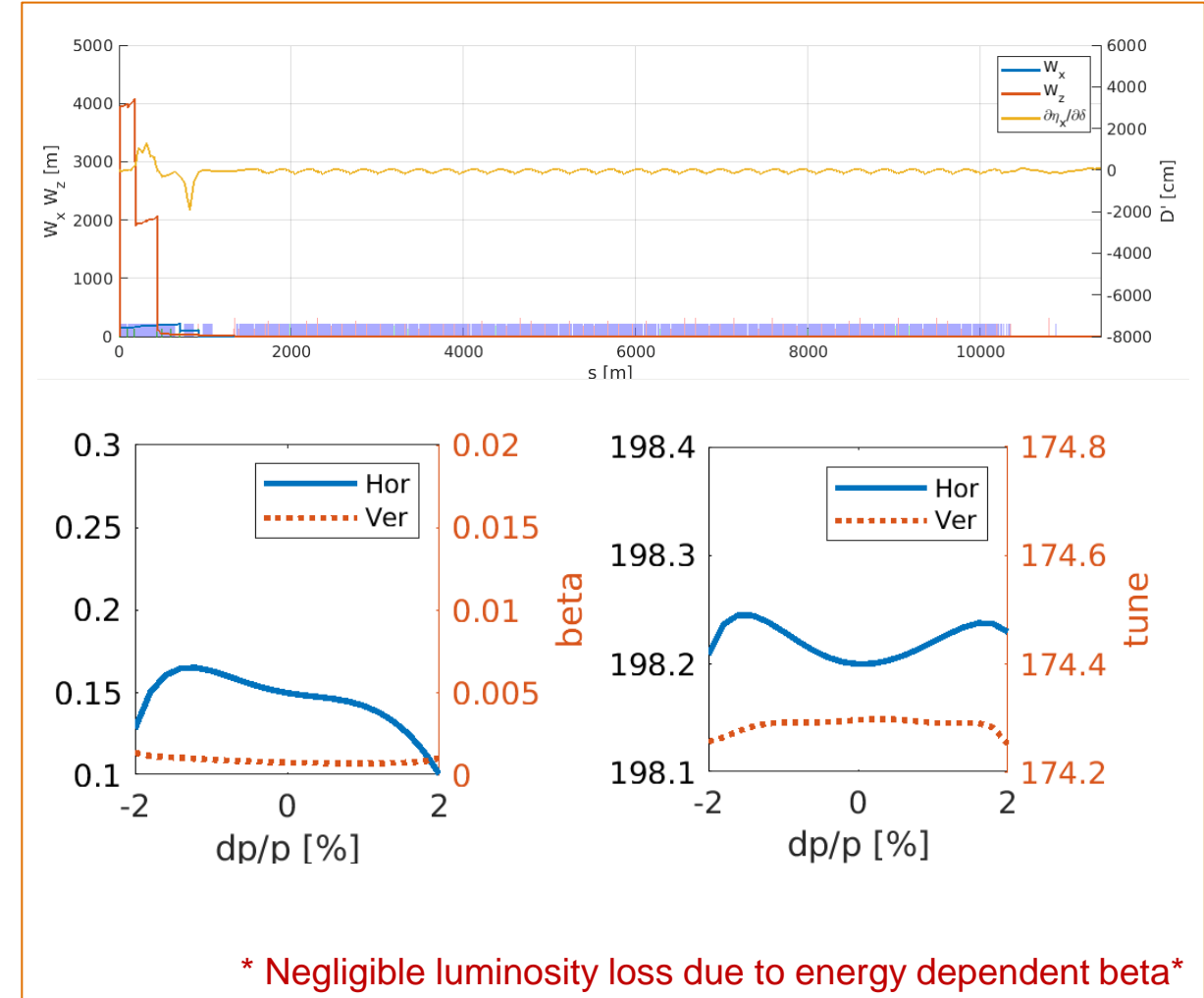
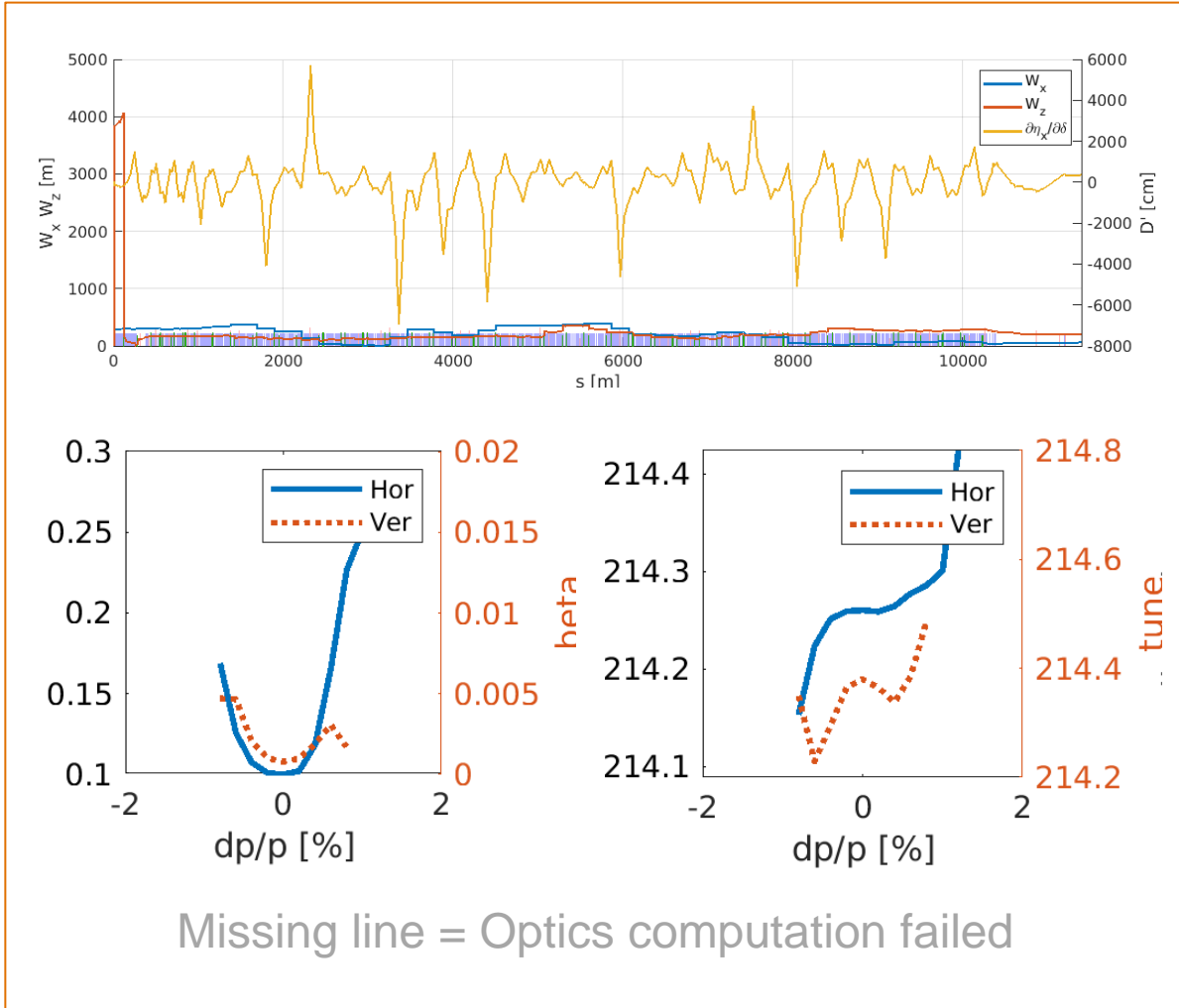


Only magnet gradients change. White boxes for baseline correspond to magnet off at Z  
 LCCO needs about half total quadrupole length and about four times less total sextupole length  
 LCCO needs about 60% of BPMs and correctors wrt baseline as well  
**LCCO requires about 13% less RF power and voltage wrt baseline**

# Off energy electron beam optics: W functions, IP bandwidth

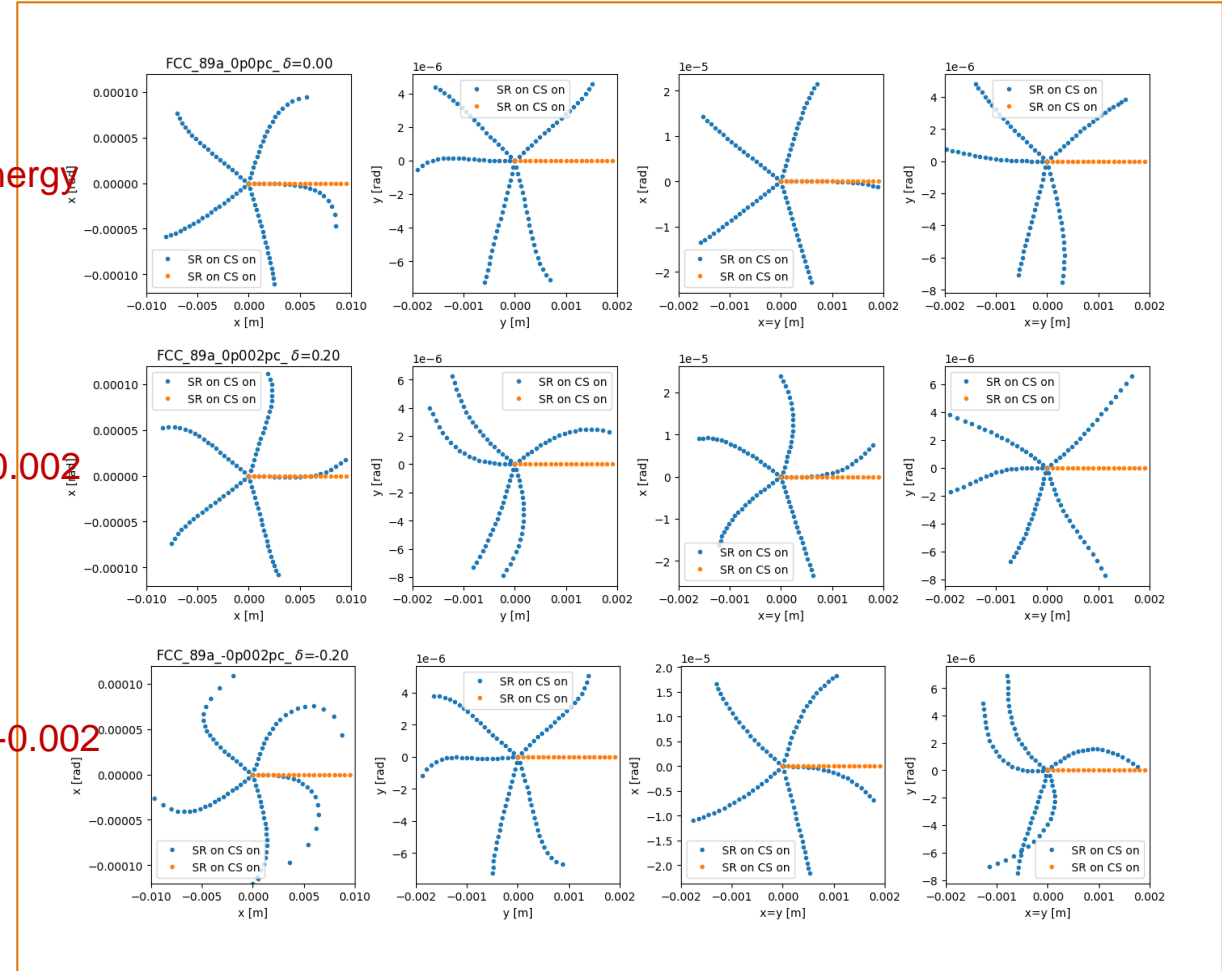
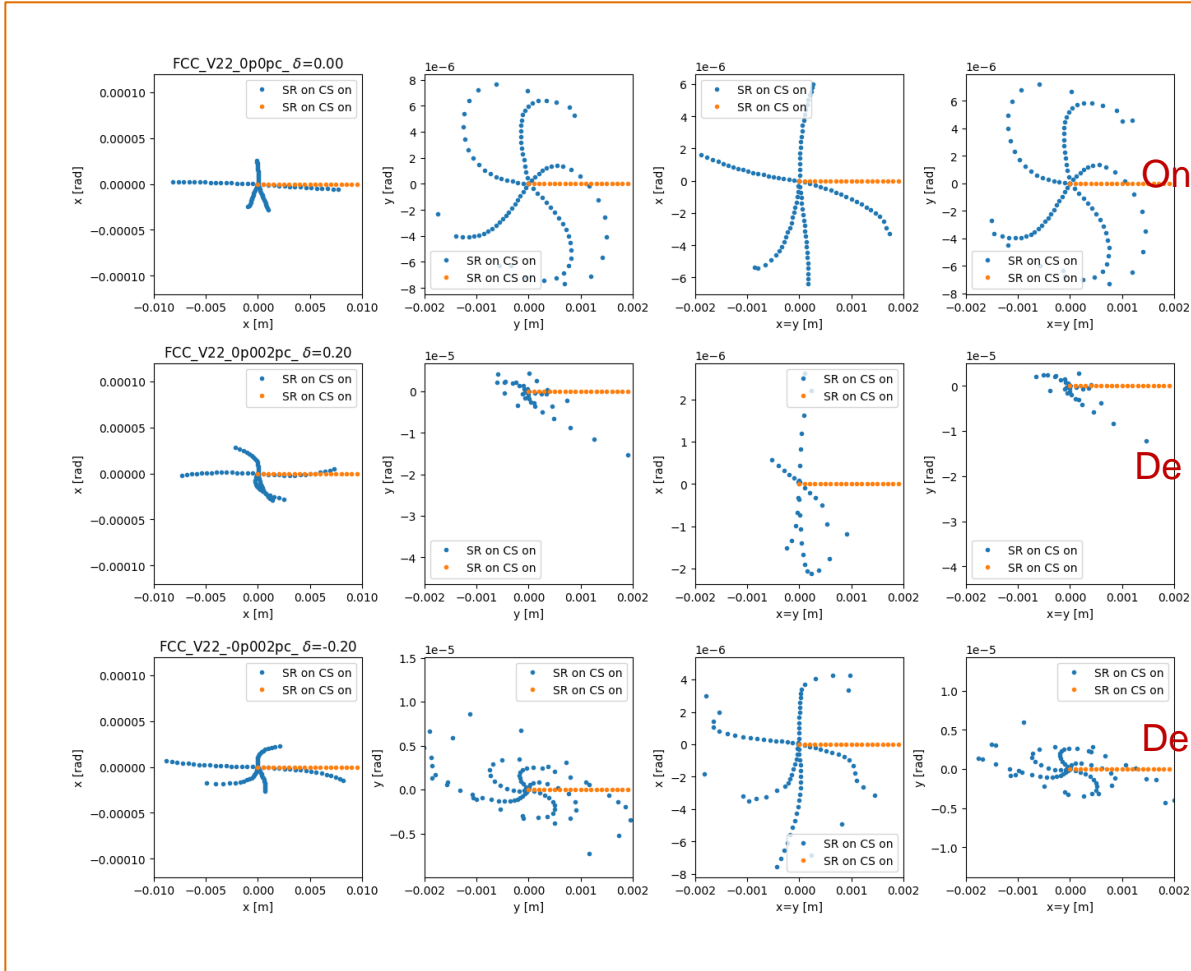
V22 (K.Oide, <https://journals.aps.org/prab/abstract/10.1103/PhysRevAccelBeams.19.111005>)

LCCO-89 (P.Raimondi, <https://indico.cern.ch/event/1326738/timetable/#45-alternative-optics-and-vari>)



# Phase space evolution over 5 turns on and off energy

No SR in dipoles (no effect)

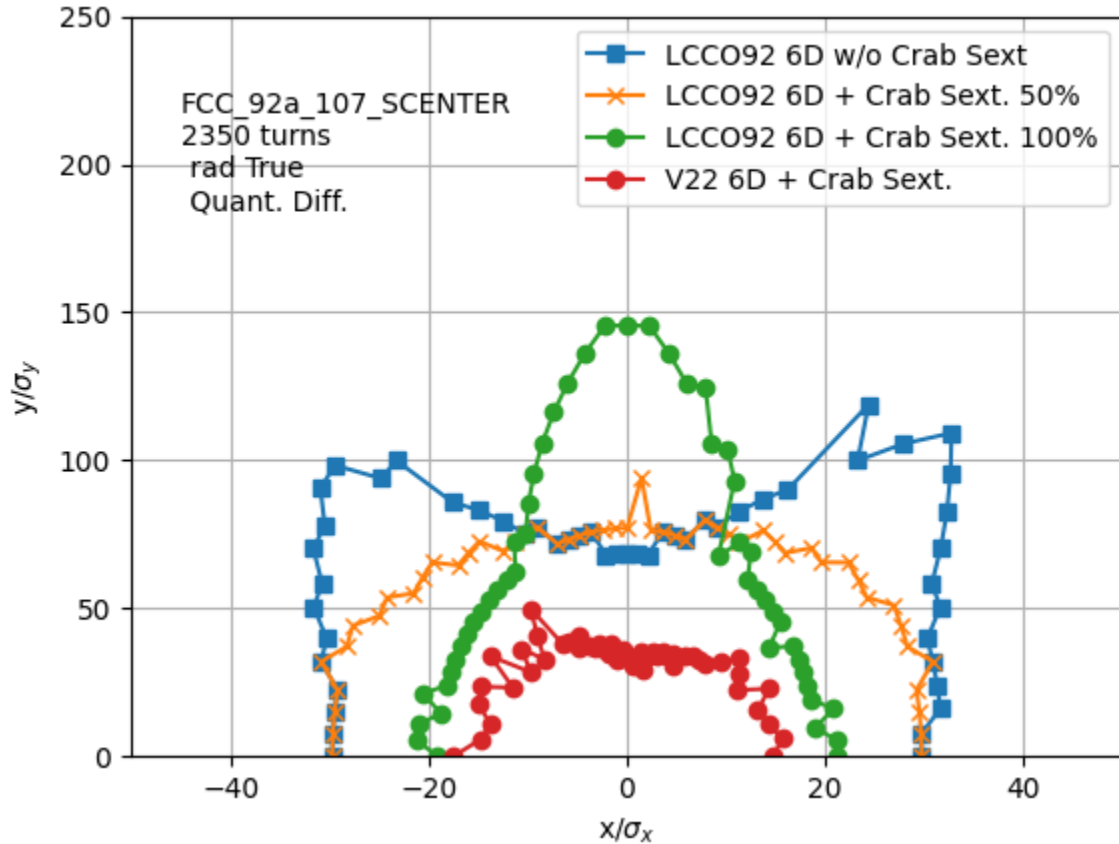


## SYNCHROTRON RADIATION AND CRAB SEXTUPOLES ON

Starfish plots provide a “quick” overview of the combined effect of all the resonant driving terms

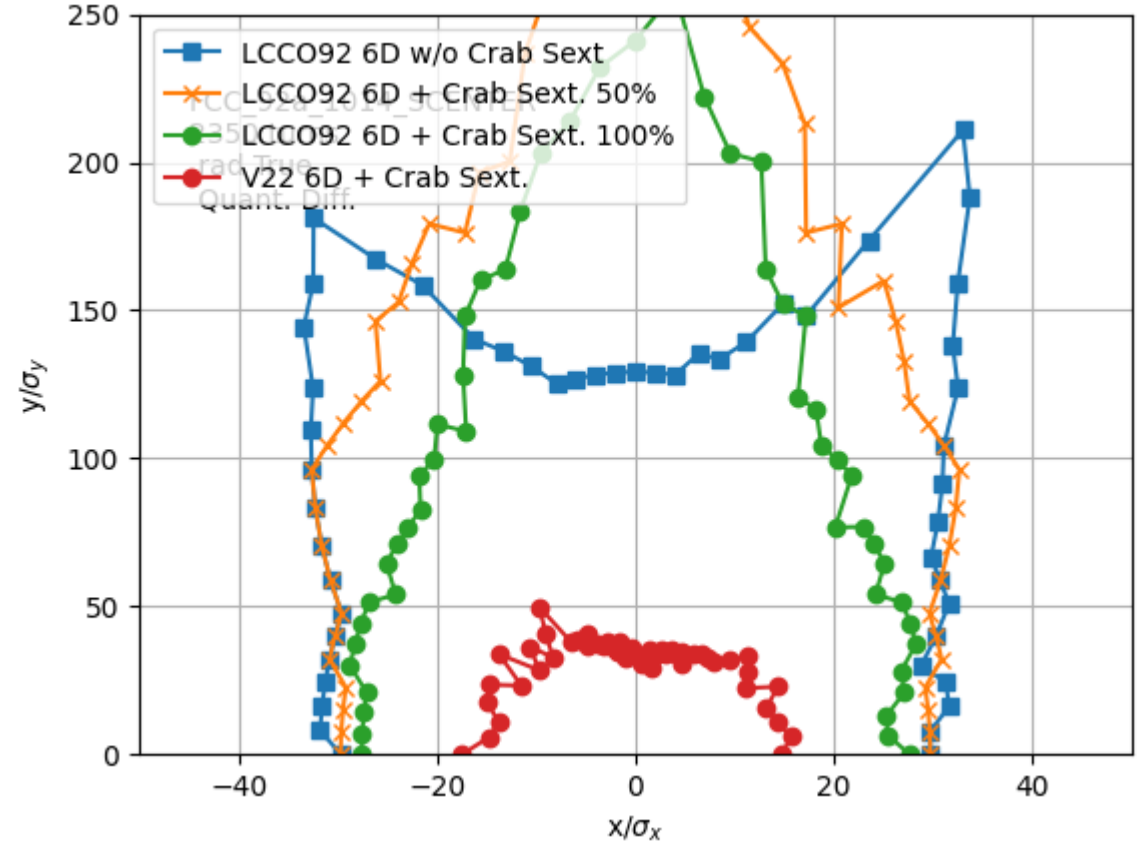
# Up to date IP beta\* and corresponding Relaxed optics LCCO92

Present baseline beta\*:  $\beta^*_h=10\text{cm}$ ,  $\beta^*_v=0.7\text{mm}$



Relaxed vertical beta:  $\beta^*_h=10\text{cm}$ ,  $\beta^*_v=1.4\text{mm}$

Relaxed beta optic obtained by changing  
2\*6 beta matching quads only at FF entrance

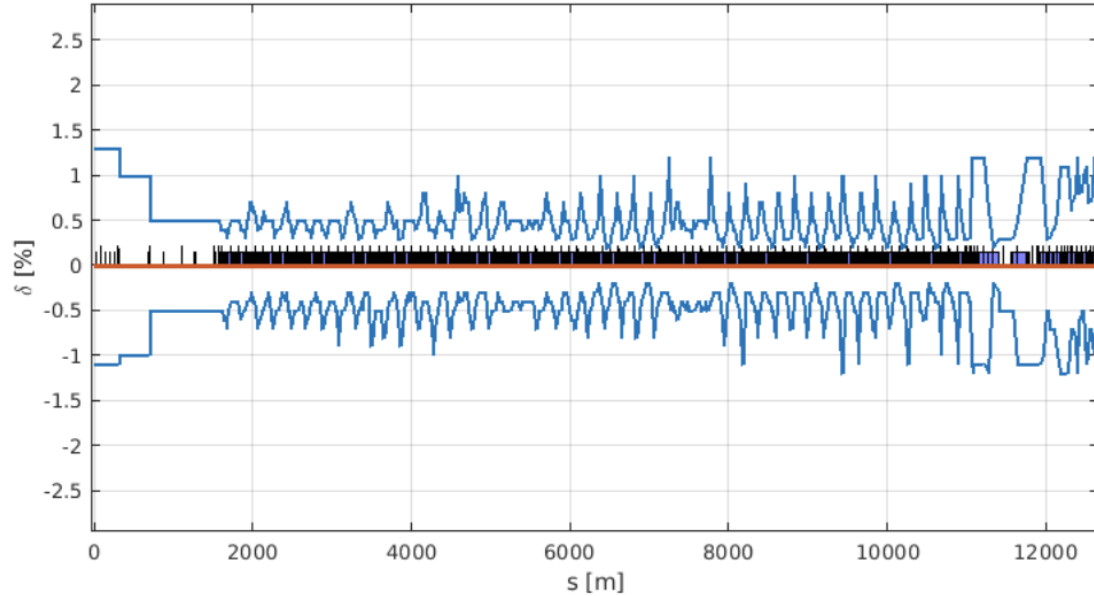


\*Decapoles settings optimized only with CS on

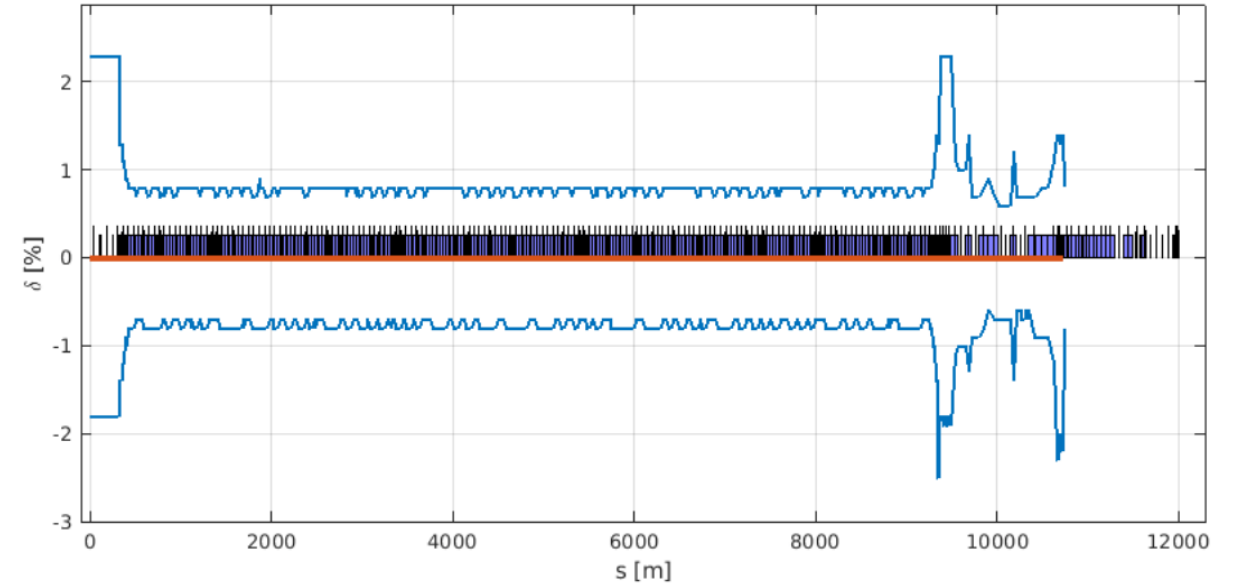
# Local momentum acceptance no synchrotron Radiation (OPTIMISTIC)

LCCO 76

EY: 1.4111 pmrad,  $V_{RF}=200\text{MV}$ ,  $I_{\text{bunch}}=0.1\text{mA}$ ,  $b_1=19.1675\text{mm}$   
rfon, rad off, 512 turns



EY: 0.97717 pmrad,  $V_{RF}=200\text{MV}$ ,  $I_{\text{bunch}}=0.1\text{mA}$ ,  $b_1=18.9909\text{mm}$   
rfon, rad off, 512 turns



6.5h

$$\tau_{Tou.,bunch} \propto \frac{\delta^3 \sqrt{\epsilon_v} \sqrt{\epsilon_h} \sigma_l}{I_{bunch}}$$

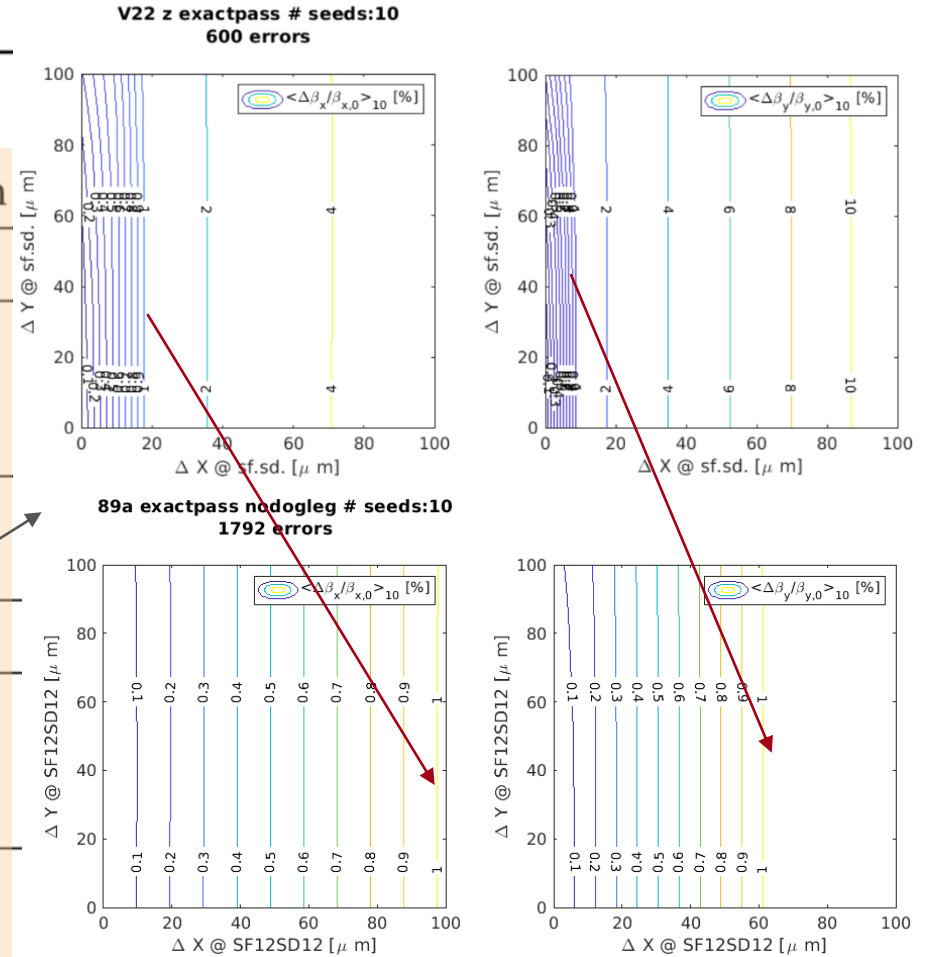
12.2h

Small momentum acceptance locations have large impact on final Vacuum and Touschek Lifetime



# Arc alignment sensitivities

| criteria                                      | $E_0$      | #    | orbit                  |                        | $\Delta\beta/\beta$ |          | $\Delta\eta$ |           |
|---|------------|------|------------------------|------------------------|---------------------|----------|--------------|-----------|
|   |            |      | H<br>100 $\mu\text{m}$ | V<br>100 $\mu\text{m}$ | H<br>1 %            | V<br>1 % | H<br>1 mm    | V<br>1 mm |
| arc quadrupoles sensitivity [ $\mu\text{m}$ ] |            |      |                        |                        |                     |          |              |           |
| V22 (.26 .38)                                 | Z          | 1420 | 1.9                    | 1.9                    | 2.9                 | 0.7      | 0.1          | 0.1       |
| LCCO89 (.20 .30)                              | Z          | 2168 | 1.7                    | 1.4                    | 5.3                 | 0.4      | 0.2          | 0.24      |
| LCCO89 (.26 .38)                              | Z          | 2168 | 2.0                    | 1.6                    | 6.1                 | 0.5      | 0.9          | 0.26      |
| V22   | $t\bar{t}$ | 2836 | 1.3                    | 1.5                    | 1.5                 | 0.5      | 0.12         | 0.2       |
| LCCO89  | $t\bar{t}$ | 2168 | 1.3                    | 0.9                    | 2.1                 | 0.45     | 1.0          | 0.3       |
| arc sextupoles sensitivity [ $\mu\text{m}$ ]  |            |      |                        |                        |                     |          |              |           |
| V22 (.26 .38)                                 | Z          | 600  | >100                   | >100                   | 17                  | 8.5      | 3.1          | 2.6       |
| LCCO89 (.20 .30)                              | Z          | 1792 | >100                   | >100                   | 97                  | 61       | 12           | 10        |
| LCCO89 (.26 .38)                              | Z          | 1792 | >100                   | >100                   | >100                | 46       | 14           | 10        |
| V22   | $t\bar{t}$ | 2336 | >100                   | >100                   | 10                  | 7.0      | 7.5          | 10        |
| LCCO89  | $t\bar{t}$ | 1792 | >100                   | >100                   | 22                  | 15       | 12           | 11        |



LCCO ARC errors sensitivities are always better (apart sextupoles induced vertical dispersion)

# Final Focus alignment sensitivity

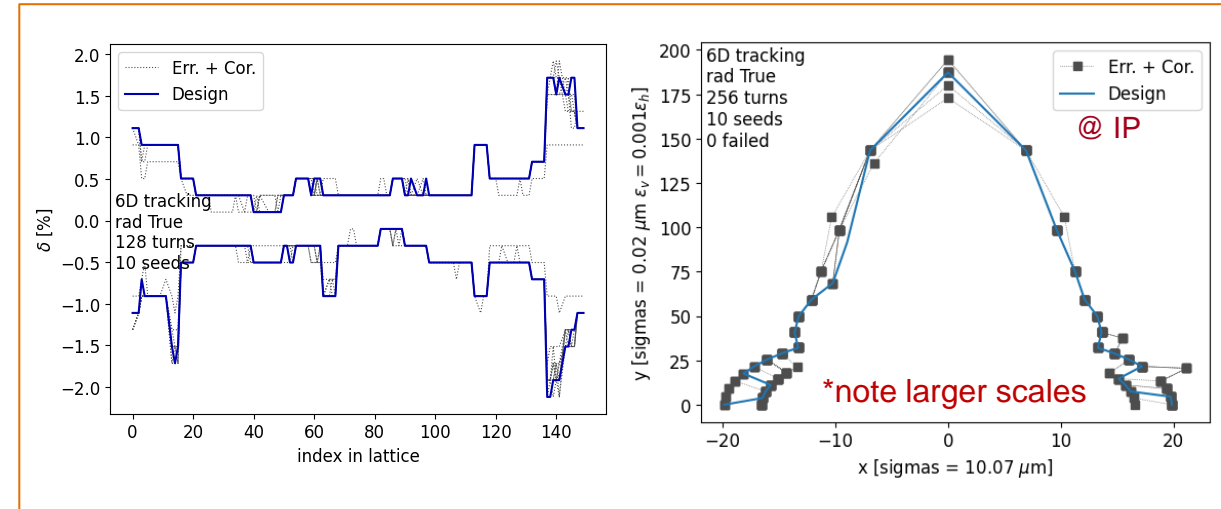
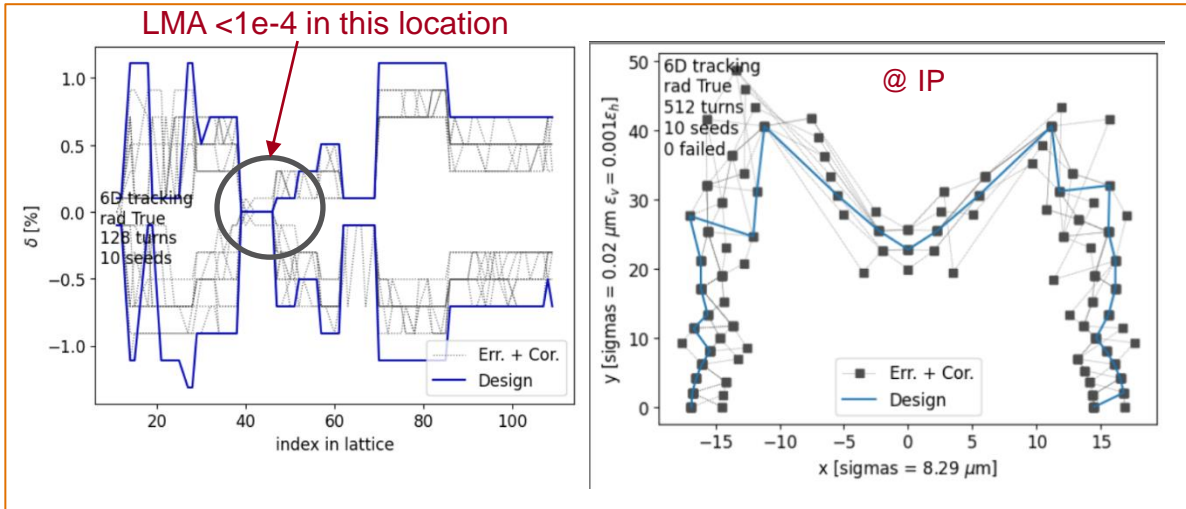
| criteria  | $E_0$      | #   | orbit                  |                        | $\Delta\beta/\beta$ |          | $\Delta\eta$   |           |
|---|------------|-----|------------------------|------------------------|---------------------|----------|----------------|-----------|
|   |            |     | H<br>100 $\mu\text{m}$ | V<br>100 $\mu\text{m}$ | H<br>1 %            | V<br>1 % | H<br>1 mm      | V<br>1 mm |
| final focus quadrupoles sensitivity to (hor., ver.) alignment [ $\mu\text{m}$ ] |            |     |                        |                        |                     |          |                |           |
| V22 (.26 .38)   | Z          | 436 | 0.8                    | 0.1                    | (1.5, 1.2)          | 0.05     | (0.025, 0.025) | 0.01      |
| LCCO89 (.20 .30)  | Z          | 532 | 0.6                    | 0.1                    | 0.3                 | <0.1     | 0.04           | 0.01      |
| LCCO89 (.26 .38)  | Z          | 532 | 0.6                    | 0.12                   | 0.6                 | <0.01    | 0.06           | <0.01     |
| V22   | $t\bar{t}$ | 480 | 2.0                    | 0.35                   | 2.1                 | 0.22     | 0.24           | 0.04      |
| LCCO89  | $t\bar{t}$ | 532 | 1.4                    | 0.25                   | 2.3                 | 0.04     | 0.24           | 0.05      |
| final focus sextupoles sensitivity to (hor., ver.) alignment [ $\mu\text{m}$ ]  |            |     |                        |                        |                     |          |                |           |
| V22 (.26 .38)   | Z          | 16  | >10                    | >10                    | >10                 | 0.25     | >10            | 1.2       |
| LCCO89 (.20 .30)  | Z          | 152 | >10                    | >10                    | >10                 | 1.1      | 8.6            | 1.8       |
| LCCO89 (.26 .38)  | Z          | 152 | >10                    | >10                    | >10                 | 0.8      | >10            | 2.0       |
| V22   | $t\bar{t}$ | 16  | >10                    | >10                    | >10                 | 0.50     | >10            | 2.6       |
| LCCO89  | $t\bar{t}$ | 152 | >10                    | >10                    | >10                 | 1.9      | >10            | 3.4       |

~4x better

Orbit in FF sextupoles has to be maintained at this level during operation

# Error Tolerances: commissioning simulations

Set errors and apply correction sequence: beam threading (first turns), orbit, tunes, optics, coupling, etc...



**10um random errors only in the ARCS quadrupoles and sextupoles already impact DA, LMA and optics parameters. Errors larger than 30um seldom make it through first turns beam threading. Final focus errors are even more demanding (<10um). This is in contrast with previous tracking simulations results\*, see tables below for V22.**

**Table 2** rms misalignment values used in simulations presented in this paper. The definition of the misalignment parameters are defined in Fig. 2. Note that values are not tolerance specifications, as there is an ongoing iterative process to determine the alignment level achievable and the acceptable machine performance

| Type             | $\Delta X (\mu\text{m})$ | $\Delta Y (\mu\text{m})$ | $\Delta \text{PSI} (\mu\text{rad})$ | $\Delta S (\mu\text{m})$ | $\Delta \text{THETA} (\mu\text{rad})$ | $\Delta \text{PHI} (\mu\text{rad})$ |
|------------------|--------------------------|--------------------------|-------------------------------------|--------------------------|---------------------------------------|-------------------------------------|
| Arc quadrupoles* | 50                       | 50                       | 300                                 | 150                      | 70                                    | 70                                  |
| Arc sextupoles*  | 50                       | 50                       | 300                                 | 150                      | 70                                    | 70                                  |
| Dipoles          | 1000                     | 1000                     | 300                                 | 1000                     | 0                                     | 0                                   |
| Girders          | 150                      | 150                      | -                                   | 1000                     |                                       |                                     |
| IR quadrupole    | 100                      | 100                      | 250                                 | 250                      | 70                                    | 70                                  |
| IR sextupoles    | 100                      | 100                      | 250                                 | 250                      | 70                                    | 70                                  |

**Table 3** rms gradient errors used in all simulations presented in this paper. Note that values are not tolerance specifications, as there is an ongoing iterative process to determine the field precision achievable and the acceptable machine performance

| Type           | Field Errors                    |
|----------------|---------------------------------|
| Arc quadrupole | $\Delta k/k = 2 \times 10^{-4}$ |
| Arc sextupoles | $\Delta k/k = 2 \times 10^{-4}$ |
| Dipoles        | $\Delta B/B = 1 \times 10^{-4}$ |
| IR quadrupole  | $\Delta k/k = 1 \times 10^{-4}$ |
| IR sextupoles  | $\Delta k/k = 2 \times 10^{-4}$ |

Work in progress to define tolerated errors and commissioning procedures.

\* T. K. Charles et al. <https://link.springer.com/content/pdf/10.1140/epjti/s40485-023-00096-3.pdf>  
 | 7th FCC-ee physics workshop | 29Jan-2Feb 2024 | S.M.Liuzzo, P.Raimondi, M.Hofer

## Some LCCO highlights

- ARC tuning nearly identical to the EBS one (highest energy ring with lowest horizontal emittance existing so far)
- FF tuning knobs are very standard and can be built accordingly to the SLC/NLC/LEP ones
- Large orthogonality of many fundamental quantities, that can be varied separately with no need to retune other quantities:
  - ARC chromaticities
  - Machine tunes
  - FF chromaticities
  - Individual IP betas
  - Individual CS pairs
  - Local FF tuning knobs
- All requirements on tolerances and stabilities for LCCO are very relaxed (M Hofer S Liuzzo)

## Summary (1)

- The LCCO beam dynamics is extremely well understood and optimized
- The understanding of the quads SR on beam dynamics has lead to unprecedented means to mitigate the related DA deterioraton. This will be potentially even more beneficial to the higher energies operation.
- DA/MA exceeds the baseline, particularly in the vertical plane.
- There is only one very well identified aberrations that makes the CS detrimental to the DA. The reduction of this effect seems possible.
- Hardware requirements for LCCO are much less demanding wrt baseline

## Summary (2)

- LCCO includes all the know-how and experience acquired in designing, building, commissioning and operating most of the high-energy and high-luminosity linear and circular colliders of the past 30 years.
- Many innovative solutions developed in the very active (and forefront) Synchrotron Radiation Accelerator community are utilized as well
- LCCO hardware requirements are in line with standard (and cheap) solutions adopted for most of the colliders built so far, in particular LEP
- LCCO is an invaluable opportunity to further progress in Accelerator Physics and push forward the frontier of High Energy Science